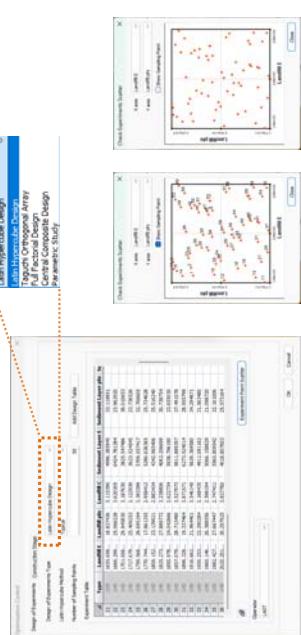




## 1.1 Optimization Options

### Design of Experiments (DOE)

- Multiple methodologies for determining the combination of design variables.
- The influence of design variables on the response can be evaluated. (For nonlinear analysis: minimum – 10 design variables, recommended – 50 design variables)



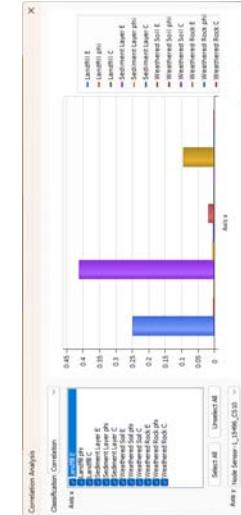
[Optimization Control – Extract Experimental Points]

**Mimis**

### 1.1 Optimization Options

#### Design of Experiments (DOE) – Post Processing

- Correlation Analysis: Determines the importance coefficient of each design variable. Used to assess how each design variable affects the accuracy of the surrogate model.
- When there are many design variables, those with correlation values close to 0 can be excluded from the design problem.
- It is possible to identify which design variables have a significant impact on each design response.



[Correlation Analysis Results]

**Mimis**

### 1.1 Optimization Options

#### Approximate Model Types

##### 1. Kriging Model

- An interpolation model that passes exactly through the experimental points.
- Combines a global regression model with local residuals.

$$Y = f'(x) \beta + r(x) \beta^{-1} (y_{exp} - F\beta)$$

- Since the most probable points need to be explored, the numerical cost of generating the surrogate model is high

##### 2. Polynomial Regression Model (Linear / Pure Quadratic / Full Quadratic / Pure Cubic)

- Surrogate equation that fits the experimental points as closely as possible
- Linear :  $y = \beta_0 + \beta_1 x_1 + \beta_2 x_2$

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1^2 + \beta_4 x_2^2 + \beta_5 x_1 x_2$$

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1^2 + \beta_4 x_2^2 + \beta_5 x_1 x_2 + \beta_6 x_1^3 + \beta_7 x_2^3$$

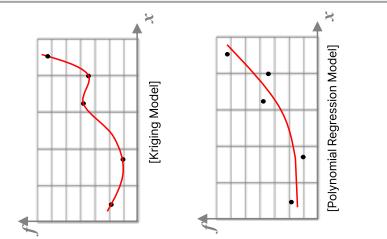
$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1^2 + \beta_4 x_2^2 + \beta_5 x_1 x_2 + \beta_6 x_1^3 + \beta_7 x_2^3$$

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1^2 + \beta_4 x_2^2 + \beta_5 x_1 x_2 + \beta_6 x_1^3 + \beta_7 x_2^3$$

- Pure Cubic:

$$y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_1^2 + \beta_4 x_2^2 + \beta_5 x_1 x_2 + \beta_6 x_1^3 + \beta_7 x_2^3$$

#### [Approximate Model Shape]



[Approximate Model Shape]

**Mimis**

### 1.1 Optimization Options

#### Approximate Model Post Processing

Approximate Model Type	Description	Approximate Model
Linear	Linear fit	
Pure Quadratic	Quadratic fit	
Full Quadratic	Quadratic fit with cross terms	
Pure Cubic	Cubic fit	
Full Cubic	Cubic fit with cross terms	

[Optimization Results Summary]

**Mimis**

Approximate Model Type	Description	Approximate Model
Linear	Linear fit	
Pure Quadratic	Quadratic fit	
Full Quadratic	Quadratic fit with cross terms	
Pure Cubic	Cubic fit	
Full Cubic	Cubic fit with cross terms	

[Optimization Results Summary]

**Mimis**

1.2 NX Interact - Automated Soil Structure Interaction between GTS NX and CIVIL NX

- Detailed **geotechnical** **interaction** (**SSI**) studies have become essential for stability assessments of critical and heavy structures, such as high-rise buildings, historic structures and bridges. These studies require seismic interoperation between structural and geotechnical software.
  - The **XN** **Impact** feature provides full compatibility between GTS NX and VNLG NX. Load combination reactions from CIVIL NX can be imported directly into GTS NX. The resulting analyses are performed, and the resulting spring data are updated in GTS NX.
  - The number of iterations can be specified for each analysis. CIVIL NX automatically runs the analyses, exports loads to GTS NX, and imports the updated soil springs into CIVIL NX, streamlining the iterative process.

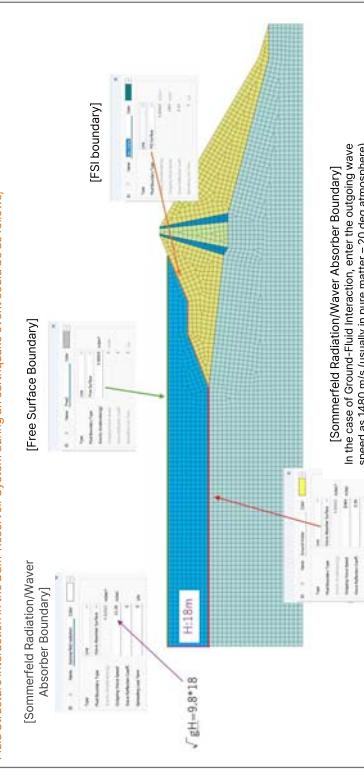
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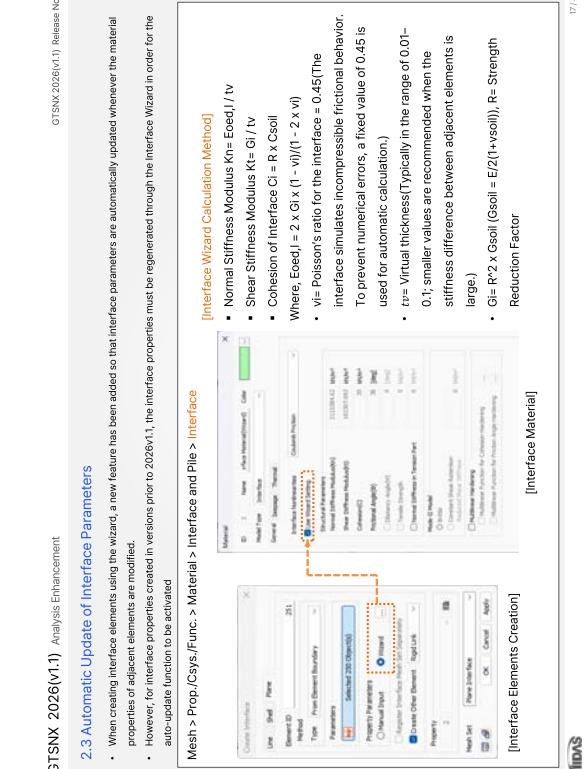
GTSNX 2026(v.1.1) Analysis Enhancement

## 2.1 Wave Absorbent Surface for Sloshing Fluid Medium

Eltiend Structure Interaction in the Dam-Reservoir System during an event



10



## 2.1 Wave Absorbent Surface for Sloshing Fluid Medium

- A wave-absorbing fluid boundary has been introduced as an additional boundary element for the fishing fluid medium.
  - In the case of Dam-Breaking and a seismic event, this element can be assigned at the far end of the reservoir. This can result in the simulation of the infinite reservoir by blocking and absorbing the reflection of waves.
  - This is essentially the Sommerfeld radiation condition, ensuring outgoing waves don't reflecting into the domain.

GTSNX 2026(v1.1) Release N

## 2.2 Addition of Normal Stiffness vs Depth for Pile Interface

Now defining Normal Stiffness Modulus vs. Depth for the Pile Interface is simpler. Users can directly input the global pile depth and corresponding Normal Stiffness Modulus. Previously, individual pile interfaces for each layer were required. This update offers two methods for defining Normal Stiffness of the Pile Interface:

1. Direct definition of Normal Stiffness Modulus for the entire pile.
2. Normal Stiffness Modulus vs. Depth.

swiss

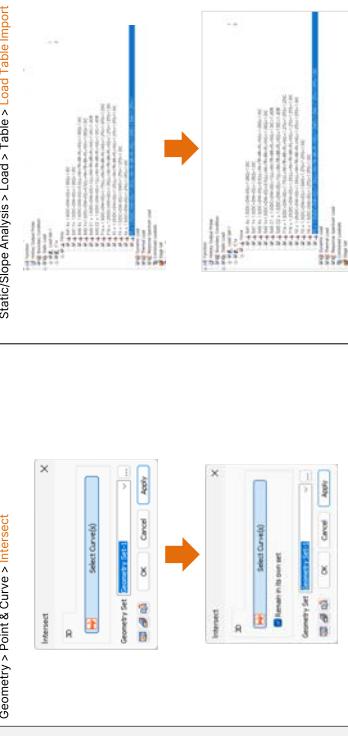


**2.11 Fixed Geometry Set for 'Intersect' Function**

When curves are intersected using the intersect function, each line is registered in its own geometry set if the 'Remain in Own Set' option is enabled.

**2.12 Enhancement in Load Table Import**

In GT-SNK, frequently used load types can be defined and imported from Excel files, or imported after definition. Previously, when load names were too long, duplication occurred, and the loads could not be retrieved correctly. This issue has been resolved by increasing the allowable string length.

25 / 42 **GT-SNK****2.13 Addition of Interface Area Column in Element Table**

- Currently, GT-SNK provides interface stress results such as Normal stress and tangential stress.
- An improvement has been made to print the interface elements area, so that the stress results can be converted into forces.
- These Normal tangential forces can then be used for calculating Total Vertical/Normal & Horizontal/Sip forces and thereby Factor of Safety Against Sliding can be determined in the case of Retaining Walls or Dams.

Mesh > Tools > Table > Element Table

Element ID	Element Type	Element Area	Element Length	Element Width	Element Height	Element Volume	Element Weight	Element Density	Element Mass
1	Element 1	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
2	Element 2	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
3	Element 3	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
4	Element 4	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
5	Element 5	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
6	Element 6	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
7	Element 7	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
8	Element 8	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
9	Element 9	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
10	Element 10	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
11	Element 11	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
12	Element 12	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
13	Element 13	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
14	Element 14	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
15	Element 15	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
16	Element 16	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
17	Element 17	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
18	Element 18	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
19	Element 19	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
20	Element 20	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
21	Element 21	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
22	Element 22	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
23	Element 23	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
24	Element 24	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
25	Element 25	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
26	Element 26	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
27	Element 27	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
28	Element 28	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
29	Element 29	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
30	Element 30	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
31	Element 31	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
32	Element 32	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
33	Element 33	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
34	Element 34	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
35	Element 35	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
36	Element 36	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
37	Element 37	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
38	Element 38	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
39	Element 39	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
40	Element 40	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
41	Element 41	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
42	Element 42	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
43	Element 43	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
44	Element 44	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
45	Element 45	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
46	Element 46	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
47	Element 47	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
48	Element 48	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
49	Element 49	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
50	Element 50	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
51	Element 51	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
52	Element 52	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
53	Element 53	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
54	Element 54	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
55	Element 55	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
56	Element 56	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
57	Element 57	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
58	Element 58	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
59	Element 59	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
60	Element 60	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
61	Element 61	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
62	Element 62	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
63	Element 63	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
64	Element 64	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
65	Element 65	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
66	Element 66	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
67	Element 67	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
68	Element 68	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
69	Element 69	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
70	Element 70	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
71	Element 71	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
72	Element 72	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
73	Element 73	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
74	Element 74	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
75	Element 75	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
76	Element 76	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
77	Element 77	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
78	Element 78	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
79	Element 79	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
80	Element 80	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
81	Element 81	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
82	Element 82	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
83	Element 83	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
84	Element 84	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
85	Element 85	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
86	Element 86	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
87	Element 87	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
88	Element 88	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
89	Element 89	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
90	Element 90	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
91	Element 91	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
92	Element 92	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
93	Element 93	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
94	Element 94	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
95	Element 95	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
96	Element 96	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
97	Element 97	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
98	Element 98	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
99	Element 99	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00
100	Element 100	1.00	2.00	1.00	1.00	2.00	1.00	1.00	2.00

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$$\text{FoS}_{\text{Sliding}} = \frac{(\mu \cdot N) + (c \cdot A)}{\sum F_{\text{Horizontal}}}$$

where:

- $\mu$ : Coefficient of friction between the dam and its foundation.
- $N$ : Net normal force acting on the base.
- $c$ : Cohesion of the foundation material.
- $A$ : Base area of the dam.

Interface forces will be helpful in determining the Fos Against Sliding - ANCOLD Guidelines for Concrete Dams

GT-SNK 2026(v1.1) Release Note

GT-SNK 2026(v1.1) Release Note